

ECE 330 Exam #1, Fall 2018 Name: Solution
 90 Minutes

Section (Check One) MWF 9 am _____ MWF 10 am _____

1. _____ / 25 2. _____ / 25
 3. _____ / 25 4. _____ / 25 Total _____ / 100

Useful information

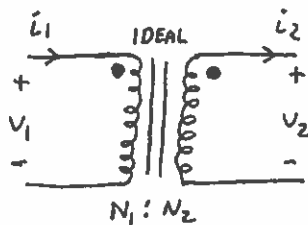
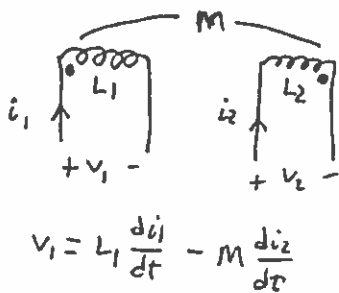
$\sin(x) = \cos(x - 90^\circ)$ $\bar{V} = \bar{Z}\bar{I}$ $\bar{S} = \bar{V}\bar{I}^* = P + jQ$ $\bar{S}_{3\phi} = \sqrt{3}V_L I_L \angle \theta$

$0 < \theta < 180^\circ$ (lag) $I_L = \sqrt{3}I_\phi$ (delta) $\bar{Z}_Y = \bar{Z}_\Delta / 3$ $\mu_0 = 4\pi \cdot 10^{-7}$ H/m
 $-180^\circ < \theta < 0$ (lead) $V_L = \sqrt{3}V_\phi$ (wye)

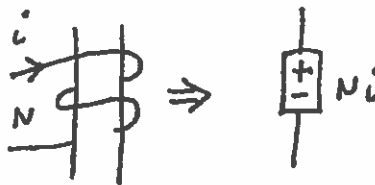
ABC sequence has A at zero, B at minus 120 degrees, and C at plus 120 degrees

$\int_C \mathbf{H} \cdot d\mathbf{l} = \int_S \mathbf{J} \cdot \mathbf{n} da$ $\int_C \mathbf{E} \cdot d\mathbf{l} = -\frac{\partial}{\partial t} \int_S \mathbf{B} \cdot \mathbf{n} da$ $\mathfrak{R} = \frac{l}{\mu A}$ $MMF = Ni = \phi \mathfrak{R}$

$\phi = BA$ $\lambda = N\phi = Li$ (if linear) $v = d\lambda/dt$ $k = \frac{M}{\sqrt{L_1 L_2}}$ 1 hp = 746 Watts

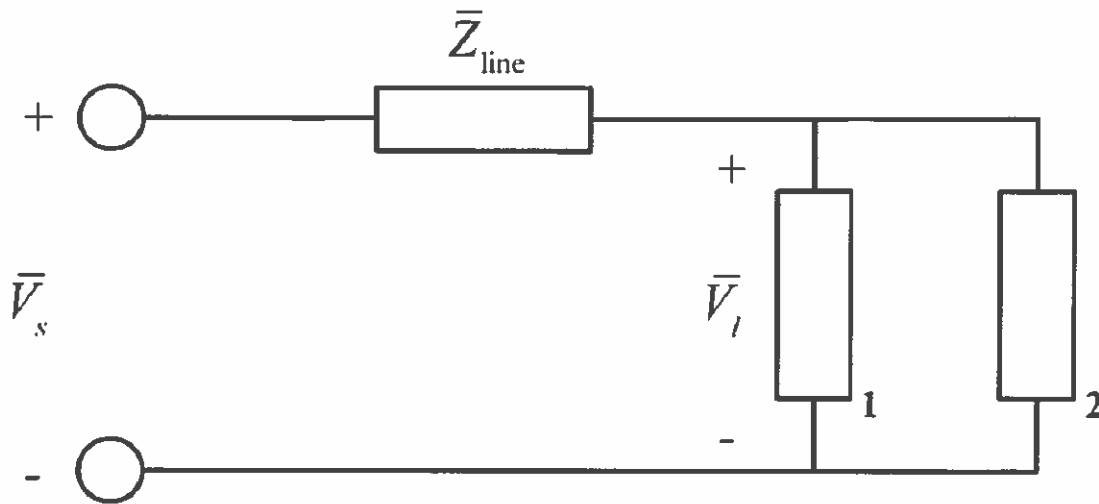


$a = \frac{N_1}{N_2}$ $N_1 i_1 = N_2 i_2$
 $\frac{v_1}{v_2} = \frac{N_1}{N_2}$



(extra paper at the end)

Problem 1:

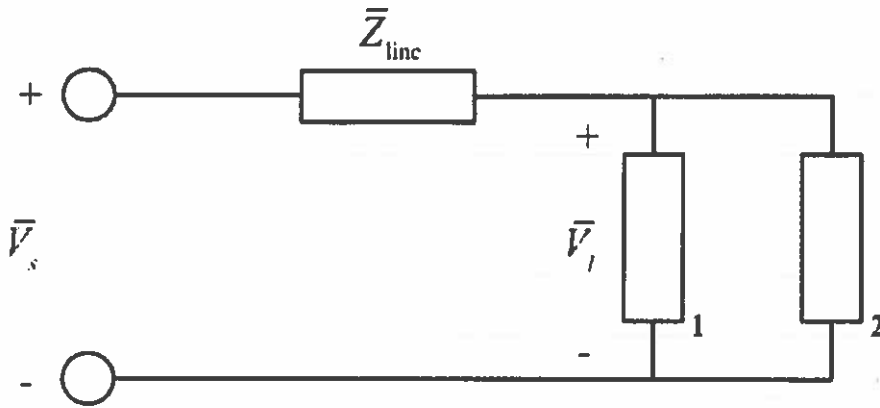


Two single-phase loads are connected in parallel to a voltage source through a feeder with impedance $\bar{Z}_{line} = 1 + j\sqrt{3} \Omega$. Load 1 consumes 1500 W of power at a power factor of 0.8 lagging. Load 2 consumes 1000 VA of power at a power factor of 0.6 lagging. The voltage at the loads is $v_l(t) = \sqrt{2}(120)\cos(377t)$ V.

Using the given values, find:

- The total complex power consumed by both loads.
- The total current supplied by the source.
- The voltage as a function of time supplied by the source $v_s(t)$.
- If a capacitor is connected in parallel with the two loads, what power must be supplied to achieve a total power factor of 0.9 lagging?

Problem 1 Solution



a) $P_1 = 1500 \text{ W}$ $PF_1 = 0.8$
 $P_1 = S_1 (PF_1) \Rightarrow S_1 = \frac{P_1}{PF_1} \Rightarrow S_1 = 1875 \text{ VA}$
 $\bar{S}_1 = 1500 + j1125 \text{ kVA}$

$S_2 = 1000 \text{ VA}$ $PF_2 = 0.6$
 $\bar{S}_2 = 600 + j800 \text{ kVA}$

$\bar{S}_{TOT} = \bar{S}_1 + \bar{S}_2 \Rightarrow \bar{S}_{TOT} = 2100 + j1925 \text{ VA}$
 $= 2848.8 \angle 42.51^\circ \text{ VA}$

b) $\bar{V}_L = 120 \angle 0^\circ \text{ V}$

$\bar{S}_{TOT} = \bar{V}_L \bar{I}_{TOT}^*$
 $\bar{I}_{TOT} = \left(\frac{\bar{S}_{TOT}}{\bar{V}_L} \right)^* \Rightarrow \bar{I}_{TOT} = 23.74 \angle -42.51^\circ \text{ A}$

c) $\bar{V}_s = \bar{Z}_{line} \bar{I}_{TOT} + \bar{V}_L \Rightarrow \bar{V}_s = (2 \angle 60^\circ)(23.74 \angle -42.51^\circ) + 120 \angle 0^\circ \text{ V}$

$\bar{Z}_{line} = 2 \angle 60^\circ$

$\bar{V}_s = 47.48 \angle 17.49^\circ + 120 \angle 0^\circ \Rightarrow \bar{V}_s = 165.295 + j14.21 \text{ V}$

$\bar{V}_s = 165.9 \angle 4.93^\circ \text{ V}$

$v_s(t) = \sqrt{2} (165.9) \cos(377t + 4.93^\circ)$

d) $Q_{TOT} = 1925 \text{ VAR} \Rightarrow Q_C = 1925 \text{ VAR}$ or 1925 VAR of capacitance added.

Problem 2. (25 points)

A balanced, symmetrical, Wye-connected, three-phase load consumes a total of 1,000 Watts (3 phase) at a voltage of 208 V (line-line). The line current is 4 Amps and the power factor is lagging.

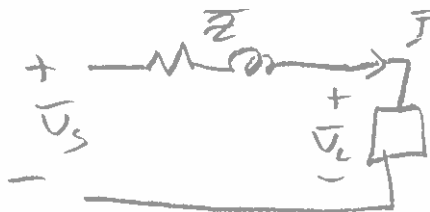
- a) Find the **capacitance** needed for use in a Delta connection across the load to lower the line current to 3 Amps while the load still consumes the same real power. Assume a 60Hz supply.

$$\begin{aligned} \bar{S}_0 &= \sqrt{3} \times 208 \times 4 \angle \theta_0 = 1000 + jQ_0 & \theta_0 &= 46^\circ \\ \bar{S}_1 &= \sqrt{3} \times 208 \times 3 \angle \theta_1 = 1000 + jQ_1 & Q_0 &= 1037 \text{ vars} \\ & & \theta_1 &= 22.3^\circ \\ & & Q_1 &= 410 \text{ vars} \\ \text{Need } 1037 - 410 &= 627 \text{ vars } 3\phi \\ 627 &= 3 \times \frac{208^2}{X_C} & X_C &= 207 \Omega = \frac{1}{2\pi 60 C} \\ & & & \boxed{C = 12.8 \mu\text{F}} \end{aligned}$$

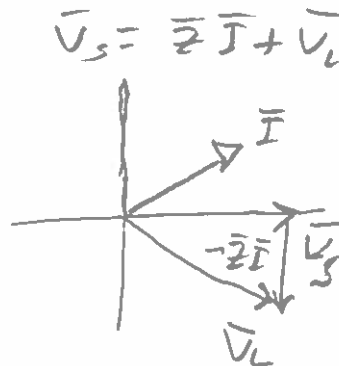
- b) What would the line current be if these same capacitors were connected in a Wye rather than a Delta?

$$\begin{aligned} Q_{\text{new}} &= 3 \times \frac{1202}{207} = 209 \text{ vars } 3\phi \\ \bar{S}_2 &= \sqrt{3} \times 208 \times I \angle \theta_2 = 1000 + j(1037 - 209) \\ &= 1000 + j828 = 1298 \angle 40^\circ \\ \boxed{I = 3.6 \text{ A}} \end{aligned}$$

- c) In the real world, the line that serves the load has a series inductive impedance. If the source voltage is fixed, the load voltage will depend on the load power and the capacitors that are added. Show with a "per-phase" phasor diagram that if enough capacitance is added, the load voltage magnitude can be larger than the source voltage magnitude.



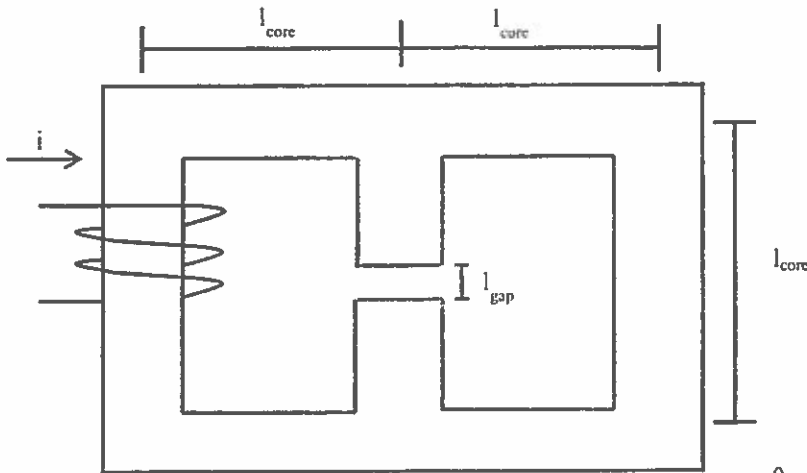
$$\bar{V}_L = \bar{V}_s - \bar{Z}\bar{I}$$



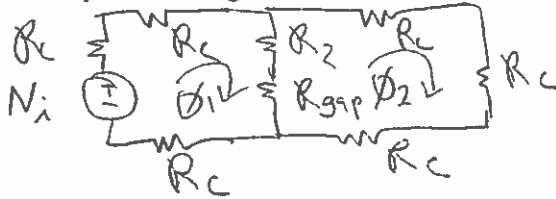
assume $\bar{Z}\bar{I} \approx V \angle 90^\circ$

Problem 3. (25 points)

Consider the iron geometry given in the figure below. Assume fringing in the air gap such that $A_{\text{gap}} = 1.1 \cdot A_{\text{core}}$, and assume the following values: $l_{\text{core}} = 10 \text{ cm}$, $l_{\text{gap}} = 0.1 \text{ cm}$, $A_{\text{core}} = 2 \text{ cm}^2$, $N = 100$, and $\mu_r = 1000$.



(a) Draw the equivalent magnetic circuit.

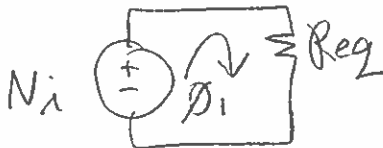


$$R_c = \frac{l}{\mu \mu_r} = \frac{0.1}{1000 \times 4\pi \times 10^{-7} \times 0.0002} = 397887 \text{ AT/W}$$

$$R_g = \frac{0.001}{4\pi \times 10^{-7} \times 0.00022} = 361716 \times 10^6 \text{ AT/W}$$

$$R_2 = \frac{(0.1 - 0.001)}{1000 \times 4\pi \times 10^{-7} \times 0.0002} = 393908 \text{ AT/W}$$

(b) Find the inductance of the coil.



$$R_{eq} = 3R_c + [(R_2 + R_g) / 3R_c]$$

$$R_g = 919906 \text{ AT/W}$$

$$R_2 + R_g = 4.01107 \times 10^6 \text{ AT/W}$$

$$R_{eq} = 2.11 \times 10^6 \text{ AT/W}$$

$$\begin{aligned} \phi_1 &= \frac{100i}{R_{eq}} & L &= \frac{N\phi}{i} = \frac{N^2}{R_{eq}} \\ & & &= 0.000473 \text{ H} \\ & & &= \underline{\underline{4.73 \text{ mH}}} \end{aligned}$$

Continued on the next page

- (c) Find the current needed to generate a flux in the middle leg of 5×10^{-6} Wb.

$$(\Phi_1 - \Phi_2) = 5 \times 10^{-6} \Rightarrow \Phi_1 = 5 \times 10^{-6} + \Phi_2 \quad \Phi_2 = \frac{MMF}{3R_c}$$

$$5 \times 10^{-6} \times (R_2 + R_g) = MMF = 20.0553$$

$$\Phi_2 = 0.000017$$

$$\Phi_1 = 5 \times 10^{-6} + 0.000017 = 0.000022$$

$$\text{Loop 1: } -Ni + 3R_c\Phi_1 + MMF = 0$$

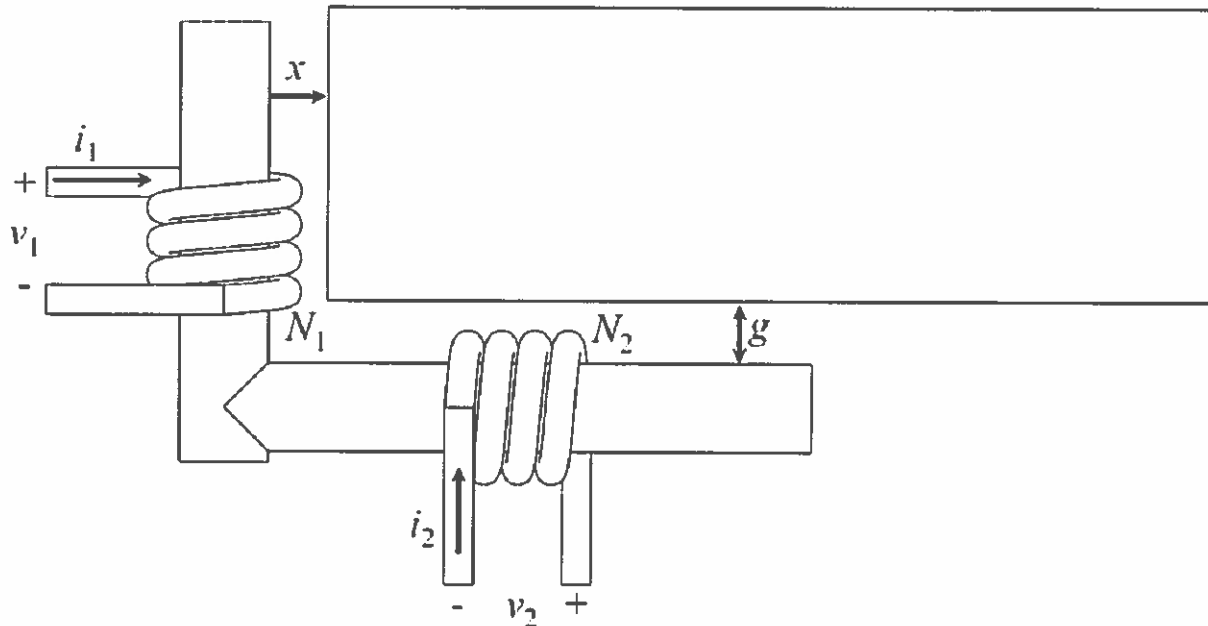
$$\underline{i} = (3R_c\Phi_1 + 20.0553) / 100 = \underline{0.463 \text{ A}}$$

- (d) Find the flux density (Wb/m^2) in the right leg corresponding to the values given in part c.

$$\Phi_2 = 0.000017$$

$$\underline{B_2} = \frac{\Phi_2}{A_2} = \frac{0.000017}{0.0002} = \underline{0.085 \text{ Wb/m}^2}$$

Problem 4: (25 points)

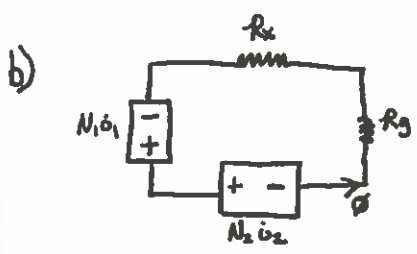
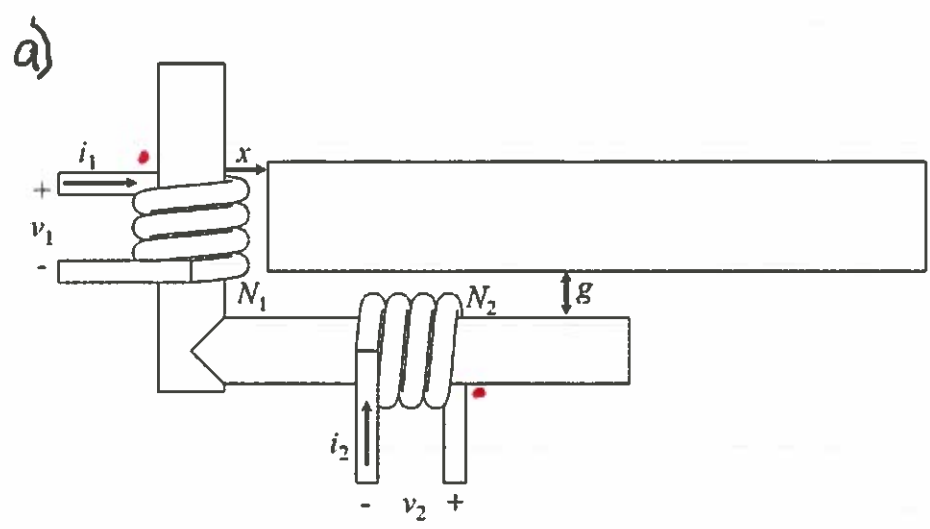


One type of magnetic actuator consists of a moving piston and two coils, as shown above. Coil 1 acts as a constant MMF source with constant current i_1 whose direction is given. Coil 2 can produce an MMF that is used to either open or close the actuator through current i_2 . The number of turns for each coil is given as N_1 and N_2 respectively. There is a constant air gap g between Coil 2 and the moving piston, whose position is given by x . The areas that the magnetic field acts through in the air gap and piston location are A_g and A_x respectively. Assume that the iron core and moving piston have infinite permeability, and that the magnetic flux acts all the way around a counter-clockwise loop.

Using the current directions and polarity definitions given:

- Find the dot convention for the given coils.
- Draw the magnetic equivalent circuit for the actuator.
- The self-inductance of coil 2, L_2 , and the mutual inductance M in terms of x , g , N_1 , N_2 , A_g , and A_x .
- Qualitatively, what happens to L_2 as the actuator opens (x increases from 0 to l): increase, decrease, or stay the same?
- Find i_2 needed for zero flux through the iron.

Problem 3 Solution



c) $N_1 \dot{i}_1 - N_2 \dot{i}_2 = \phi (R_g + R_x)$ $R_g = \frac{g}{\mu_0 \mu_r A_g}$
 $N_1 \dot{i}_1 - N_2 \dot{i}_2 = \phi (R_g + R_x)$ $R_x = \frac{x}{\mu_0 \mu_r A_x}$

$$\phi = \frac{N_1 \dot{i}_1 - N_2 \dot{i}_2}{R_g + R_x}$$

$$\phi = \frac{N_1 \dot{i}_1 - N_2 \dot{i}_2}{\frac{g}{\mu_0 \mu_r A_g} + \frac{x}{\mu_0 \mu_r A_x}}$$

$$\lambda_2 = \frac{N_1 N_2 \dot{i}_1 - N_2^2 \dot{i}_2}{\frac{g}{\mu_0 \mu_r A_g} + \frac{x}{\mu_0 \mu_r A_x}} \Rightarrow \lambda_2 = \frac{\mu_0 \mu_r A_g}{g + x \left(\frac{A_g}{A_x} \right)} [N_1 N_2 \dot{i}_1 - N_2^2 \dot{i}_2]$$

$$\lambda_2 = M \dot{i}_1 - L_2 \dot{i}_2$$

$$L_2 = \frac{N_2^2}{\frac{g}{\mu_0 \mu_r A_g} + \frac{x}{\mu_0 \mu_r A_x}} \Rightarrow L_2 = \frac{\mu_0 \mu_r A_g N_2^2}{g + x \left(\frac{A_g}{A_x} \right)}$$

d) As \$x\$ increases, \$L_2\$ decreases

e) $\phi = \frac{N_1 \dot{i}_1 - N_2 \dot{i}_2}{R_x + R_g}$ $\phi = 0$
 $N_1 \dot{i}_1 - N_2 \dot{i}_2 = 0 \Rightarrow \dot{i}_2 = \left(\frac{N_1}{N_2} \right) \dot{i}_1$